Welding Metallurgy

Arc Physics and Weld Pool Behaviour

Lecture Topics

- Heat sources for welding
- Welding arcs as heat sources
 - The cathode, arc column and anode
 - Heat transfer from arcs, arc efficiency
- Weld pool behaviour
 - Heat input for melting, melting efficiency
 - Forces motion and temperatures in the weld pool

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Heat Sources for Welding

- Heat sources for welding include:
 - exothermic reactions (flames and thermit)
 - arcs
 - electrical resistance heating
 - radiant energy (electron beam, laser)
- Transferred power is the rate at which energy is delivered per unit time
- Energy density is the transferred power per unit area of contact between the heat source and work
- Energy density is a measure of the "hotness" of the source
- The development of welding processes has largely depended on availability of high energy density heat sources

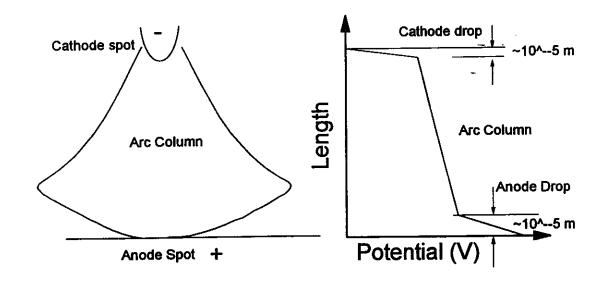
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Welding Arcs as Heat Sources

- The welding arc is a high current, low-voltage discharge
- In the arc:
 - electrons are evaporated from the cathode
 - transferred through a region of hot, ionized gas
 - and condensed at the anode.
- The arc may be divided into five parts
 - the cathode spot
 - the cathode drop zone
 - the arc column
 - the anode drop zone
 - the anode spot

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The Welding Arc



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Electron Interactions

- The energy required to evaporate one electron from a metal surface is known as the work function
- Conversely when an electron condenses in the surface_it releases this energy

Metal	Work Function (eV)	First ionization potential (V)
Aluminum	4.0	5.96
Barium	2.1	5.19
Calcium	2.2	6.09
Соррег	4.3	7.68
Iron	4.5	7.83
Nickel	5	7.61
Potassium	2.2	4.3
Tungsten	4.5	8.1

The Cathode

- Thermionic cathodes operate at high temperatures such that (e.g. GTAW) electrons are evaporated from the cathode.
- The energy required is derived from incoming positive ions that are accelerated through the cathode drop region
- The cathode loses heat through the electron work function, electron thermal energy, and by conduction through the electrode and
- The energy balance is:

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$$V_C I_{=}(\phi_e + \frac{3 kT}{2 e})I_{+}q_e$$

V_c = Cathode drop potential

= Arc current

 Φ_e = Cathode work function

k = Bolztmann's constant

T = Temperature (K)

e = Electron charge

qe = Heat loss to electrode

Non-Thermionic Cathodes

- Non-thermionic cathodes are those in which the temperature is too low for thermionic emission of electrons, i.e. on non-refractory metals.
- Where oxide films exist, the cathode appears to operate by positive ions collecting on the surface, setting up a strong electric field through the oxide, and causing electron emission through the oxide
- The general effect is to strip oxides from the surface (exploited in AC welding of Aluminum)
- Little is known about slag-covered cathodes that exist in flux-shielded processes

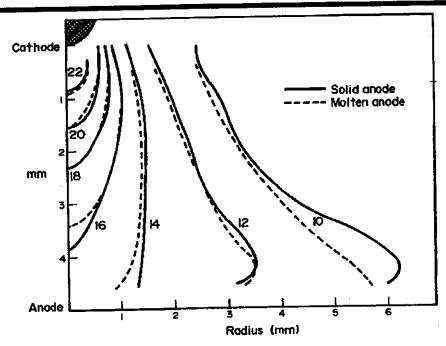
The Arc Column

- The gas in the space between the cathode and anode is at high temperature (10⁴ K), sufficient for it to be highly ionized and electrically conductive
- The arc column is electrically neutral, i.e. the number of positive and negative charges in a given volume balance
- Most of the current is carried by electrons, since they are smaller and more mobile
- The axial potential gradient in the arc column is relatively low, 10^2 to 10^3 V/m.
- The energy generated in the arc column is $q_p = V_p I$
- Heat losses in the column are mostly due to convection in the "plasma jet"

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GTAW Arc Plasma Temperatures

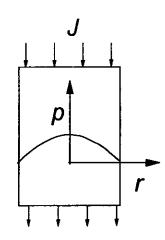


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Arc Column Plasma Jet

In a static conducting cylinder, the interaction between the current and its self-induced magnetic field produces a radial pressure.

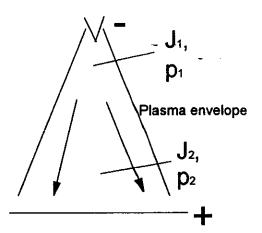
$$\rho = \frac{\mu_0 J^2}{4} (R^2 - r^2)$$



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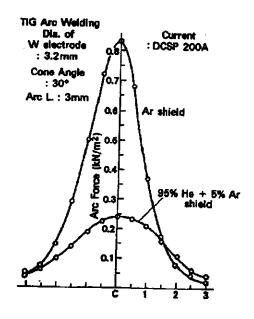
Arc Column Plasma Jet

- The radius of the arc column usually varies along the length
- The greater current density J in the constricted region produces an axial pressure gradient
- The pressure gradient causes net flow through the arc.
- Maecker suggested that the jet stagnation pressure is approximately equal to the pressure in the constricted region
- The strength of the jet depends on current and electrode vertex angle
- Flow velocities and stagnation pressures can reach 10² m/s and 1 kPa, respectively



$$\frac{1}{2}\rho v^2 = \frac{\mu_0 J_1^2}{4}$$

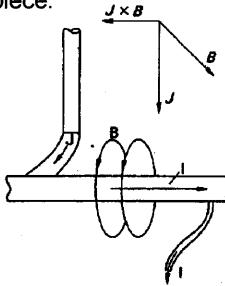
GTAW Plasma Jet Pressure



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Arc "Blow"

Arc blow results from interaction with magnetic fields in the workpiece. $J \times B$



The Anode

- At the anode, electrons are accelerated across the anode fall potential and condense in the metal surface, thereby releasing energy
- The anode loses energy by radiation but also gains energy by radiation and convection from the plasma
- The energy balance at the anode is:

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(1-m)q_A = (\phi_A - \frac{3kT}{2e} + V_A)I + nq_p
q_a = \text{heat input to workpiece (anode)}
m = \text{fractional heat loss by radiation}
\phi_a = \text{anode work function}
k = \text{Boltzmann's constant}
T = \text{electron temperature}
e = \text{electron charge}
VA = \text{anode fall potential}
| = \text{arc current}
| nq_p = \text{heat transfer from arc column}
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Arc Heat Generation

- The heat generated by the arc may be divided into three parts:
 - the heat generated at the cathode

$$ac = VcI \quad (\sim 20\%)$$

- the heat generated in the arc column

$$q_p = V_p I \qquad (\sim 20\%) - \cdot$$

- the heat generated at the anode

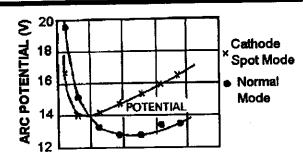
$$qa = Va! \quad (\sim 60\%)$$

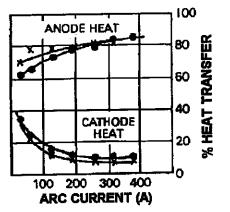
- The total arc energy is $VI = (V_c + V_p + V_a)I$
- Arc efficiency, assuming the work is the anode, is:

$$\eta = 1 - \frac{q_e + (1 - n)q_p + mq_a}{V}$$

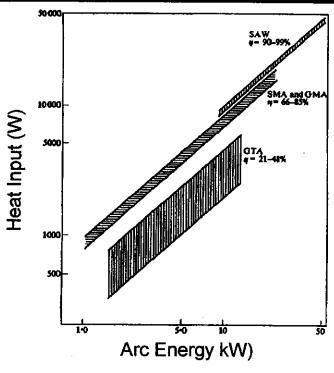
With consumable electrodes, q_c is transferred to the workpiece, increasing arc efficiency

GTAW V-I & Heat Transfer Characteristics



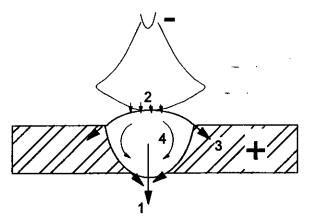






Forces Acting on the Weld Pool

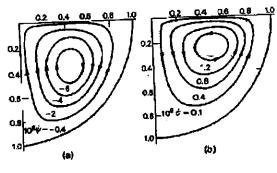
- 1. Gravity
- 2. Arc Pressure
- 3. Surface Tension
- 4. Lorenz (electromagnetic) forces

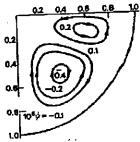


Motion in the weld pool

Theoretical MHD flow streamlines for various current source and sink distributions

The Lorenz (JxB) magnetohydrodynamic forces vary as the square of current.





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Surface Tension Flows

- Certain elements in the weld pool such as sulphur and oxygen are "surface active" and affect surface tension (like soan)
- Surface tension gradients can drive flows in the liquid metal (Marangoni convection)
- Thus weld penetration can depend on base metal composition. This has been a particular problem in GTAW welding of stainless steels, e.g. tubing, where a precise weld bead shape is desired.

		 		
				
		 		
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Effects of Weld Pool Motion

- Weld pool composition tend to be homogenized by fluid motion
- The weld pool is relatively transparent to heat flow
- However, the exact cross-section of the weld bead is difficult to predict and may vary even if welding conditions are nominally constant.